

<sup>5</sup> Hunziker, R. R., "Missile position and velocity estimation from radar and inertial sensors data," Technical Analysis Office TR 63-8, Hughes Aircraft Co., Washington, D. C. (August 1963).

<sup>6</sup> Hunziker, R. R., "Estimation of rocket position and velocity during boost with one tracking radar," Technical Analysis Office TR63-1, Hughes Aircraft Co., Washington, D. C. (April 1963).

<sup>7</sup> Swerling, P., "Optimum linear estimation for random processes as the limit of estimates based on sampled data," Inst. Radio Engrs. WESCON Conv. Record, Part 4, Inform. Theory, pp. 158-163 (August 1958).

<sup>8</sup> Hunziker, R. R., "Effects of atmospheric horizontal inhomogeneity upon position and velocity determination by CW radar tracking systems," RCA Systems Analysis TDR-62, Air Force Missile Test Center (December 1961).

<sup>9</sup> Smith, E. G. and Snodgrass, R. L., "Real-time impact prediction for range safety at the atlantic missile range," RCA Mathematical Services TM-62-8, Air Force Missile Test Center (June 1962).

## A Compatibility Equation for Nonequilibrium Ionization

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AN expression of compatibility, independent of the electron collision frequency, is developed from the electron heating equation (discussed in Ref. 1) and the Saha equation. By using this compatibility relation, one may compute the profiles of electron temperature, plasma electrical conductivity, and electric field, between the anode and cathode of moderate pressure plasma devices (such as a diode or an MHD generator), once the neutral particle temperature profile and the current density have been measured. The current passing through any plane parallel to the electrodes is assumed constant. The influence of nonuniformities due to insulator walls is neglected. Radiation losses are neglected. As a first approximation, electron diffusion is also neglected.

Starting with the electron heating equation in which very steep spatial gradients are neglected,

$$j^2/\sigma = n_e \nu_e (2m_e/m_n) \delta (\frac{3}{2}kT_e - \frac{3}{2}kT_n) \quad (1)$$

where  $j$  is the current density,  $\sigma$  the plasma scalar electrical conductivity,  $n_e$  the electron density,  $\nu_e$  the electron collision frequency, and  $m_e$  the electron mass.  $m_n$  is the average heavy particle mass ( $2m_e/m_n$  represents the average fraction of energy loss per electron per elastic heavy particle collision),  $\delta$  the loss factor that accounts for inelastic collisions and radiation losses ( $\delta$  is near unity for monatomic particles but is very large for polyatomic particles, as discussed in Ref. 2),  $k$  the Boltzmann constant,  $T_e$  the average electron temperature, and  $T_n$  the average neutral particle temperature.

The scalar conductivity equation is

$$\sigma = (ne^2/m_e \nu_e) \quad (2)$$

where  $e$  is the electron charge.

The electron collision frequency is eliminated by combining Eqs. (1) and (2). The resulting expression is then substituted into the Saha equation:

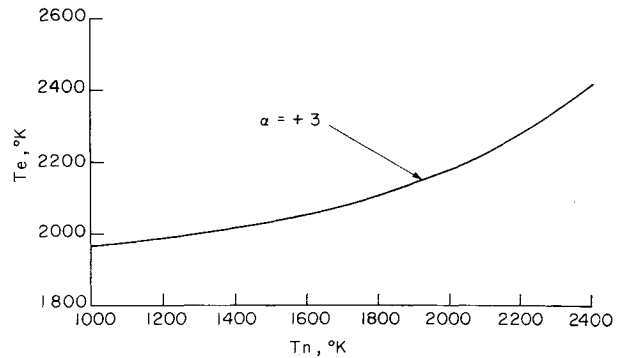


Fig. 1. Electron temperature vs neutral particle temperature for  $\alpha = 3$ .

$$\frac{n_e^2}{n_s} = \left( \frac{2\pi m_e k T_e}{h^2} \right)^{3/2} e^{-E_0/kT_e} \quad (3)$$

where  $n_s$  is the number density of ionizable particles (in the case of a seeded plasma,  $n_s = X_s n_n$ , where  $X_s$  is the mole fraction of seed in  $n_n$  neutral particles),  $h$  is the Planck constant, and  $E_0$  is the ionization potential. Note that Eq. (3) is valid when  $n_e \ll n_s$  and when the ratio of the statistical weights is equal to unity.

This resulting expression (the compatibility equation) is found to be

$$j^2 = \left( \frac{3e^2 \delta}{m_n} \right) (X_s P_n) \left( \frac{T_e}{T_n} - 1 \right) \left( \frac{2\pi m_e k T_e}{h^2} \right)^{3/2} e^{-E_0/kT_e} \quad (4)$$

For convenience of computation, Eq. (4) is rearranged:

$$\frac{5040 E_0}{T_e} - \log \left( \frac{T_e}{T_n} - 1 \right) - 1.5 \log T_e = 8.05107 - \alpha \quad (5)$$

where

- $\alpha = \log(j^2 M_n / \delta X_s P_n)$
- $j$  = current density, amp/cm<sup>2</sup>
- $M_n$  = average neutral particle atomic weight
- $P_n$  = static pressure, atm
- $T_n$  = neutral particle static temperature, °K
- $T_e$  = average electron temperature, °K
- $E_0$  = ionization potential, ev

Consequently, when  $\alpha$  and  $T_n(x)$  are measured,  $T_e(x)$  can be computed from Eq. (4). (For convenience, a plot of  $T_n$

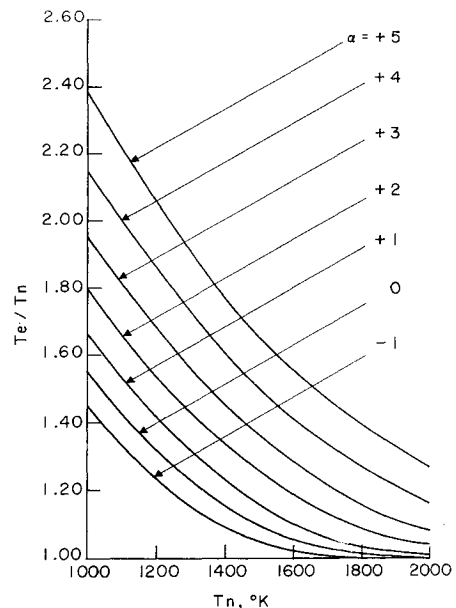


Fig. 2. Temperature ratio vs neutral particle temperature for various  $\alpha$ .

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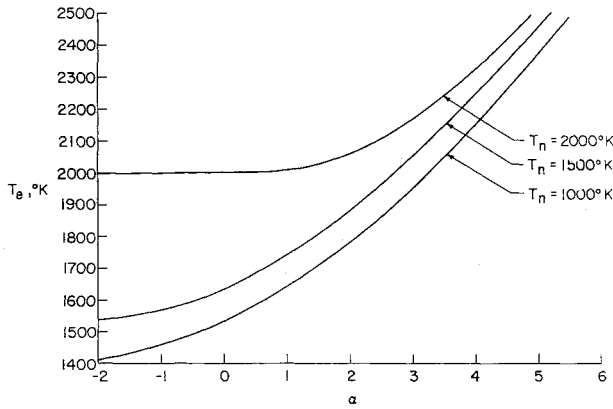


Fig. 3  $T_e$  vs  $\alpha$  for various neutral particle temperatures.

vs  $T_e$  can be computed for various  $T_e$ .) Here,  $x$  represents the normal distance from either of the electrodes. The profile of  $T_e$  can then be used to compute  $n_e(x)$ ,  $\sigma(x)$ , and  $E(x)$  between the electrodes. The more positive  $\alpha$ , the more out of equilibrium are the electrons from the heavy particles. Figure 1 shows  $T_e$  vs  $T_n$  necessary for  $\alpha = +3$  (if  $M_n \sim 40$ ,  $X_s \sim 4 \times 10^{-3}$  and  $P_n \sim 1$  atm, the  $j$  would be around 0.3 amp/cm<sup>2</sup>). It is interesting to note that the electron temperature boundary layer is usually less steep than that of the heavy particles. However, this electron temperature profile can still create a variation in the scalar conductivity, which will in turn create apparent electrical sheaths near the electrodes and thus reduce the main stream electric field. Factors that reduce  $\delta$  (such as impurities raising the value of  $\delta$ ) will make this effect more severe. Figure 2 is a typical convenient graphical representation of the compatibility equation which can be used to quickly compute  $T_e(x)$  once  $T_n(x)$  and  $\alpha$  are measured. Figures 3 and 4 show the functional dependence of  $T_e$  and  $n_e^2/(n_s - n_e)$  upon  $\alpha$ , respectively.

A corresponding expression is derived for the electron density. Recall the logarithmic form of the Saha equation:

$$\frac{5040 E_0}{T_e} - 1.5 \log T_e = 15.38274 - \log \frac{n_e^2}{n_s - n_e} \quad (6)$$

The logarithmic form of the compatibility equation is rearranged:

$$\frac{5040 E_0}{T_e} - 1.5 \log T_e = 8.05107 - \alpha + \log \left( \frac{T_e}{T_n} - 1 \right) \quad (5')$$

The ideal gas law is used:

$$n_s = 0.734 \times 10^{22} (X_s P_n / T_n) \quad (7)$$

Note that

$$\alpha \equiv \log_{10}(j^2 M_n / X_s P_n)$$

Then, for the condition  $n_e \ll n_s$ , Eqs. (5) and (6) are combined to yield

$$n_e = 4.0 \times 10^{14} \left( \frac{j^2 M_n}{\delta T_n} \right)^{1/2} 10^{-1/2 \log[(T_e/T_n) - 1]}, \frac{\#}{\text{cm}^3} \quad (8)$$

where  $j$  is in amperes per square centimeters and  $T_n$  is in degrees Kelvin. For the region  $1.3 < T_e/T_n < 3.0$ , Eq. (8) can be approximated within a factor of 2 by the following expression†:

$$n_e = 4.0 \times 10^{14} j (M_n / T_n)^{1/2} \quad \#/\text{cm}^3 \quad (9)$$

† At  $T_e/T_n = 2$ , Eq. (8) reduces exactly to Eq. (9).

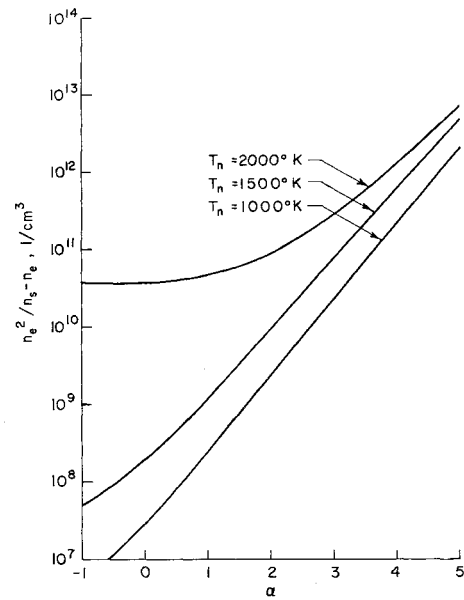


Fig. 4  $n_e^2/(n_s - n_e)$  vs  $\alpha$  for various neutral particle temperatures.

The plasma scalar conductivity can then be calculated from the hard sphere model in which the electrons are assumed to have a Maxwellian distribution:

$$\sigma_p = \frac{4.528 \times 10^{-10} n_e}{T_e^{1/2} \sum_i n_i Q_{ei}} \frac{\text{mho}}{\text{cm}} \quad (10)$$

where  $Q_{ei}$  is the elastic electron collision cross section for the  $i$ th neutral particle species in square centimeters,  $T_e$  is in degrees Kelvin,  $n_e$  is in electrons per centimeters cubed,  $n_i$  is in electrons per centimeters cubed. Since  $X_i \equiv n_i/n_n$  and  $n_n = 0.734 \times 10^{22} (P_n/T_n)$ , from the ideal gas law,

$$\sigma_p = \frac{4.528 \times 10^{-32}}{0.734} \left( \frac{T_n n_e}{T_e^{1/2} P_n \sum_i X_i Q_{ei}} \right) \quad (11)$$

Combining Eqs. (8) and (11),

$$\sigma_p = 2.47 \times 10^{-17} \frac{j}{P_n} \left( \frac{M_n T_n}{\delta T_e} \right)^{1/2} \frac{10^{-12 \log[(T_e/T_n) - 1]}}{\sum_i X_i Q_{ei}} \quad (12)$$

where  $\sigma_p$  is in ohms per centimeter.

Consequently, the associated electric field is

$$\frac{j}{\sigma_p} = 4.06 \times 10^{16} P_n \left( \frac{\delta T_e}{M_n T_n} \right)^{1/2} \frac{\sum_i X_i Q_{ei}}{10^{-1/2 \log[(T_e/T_n) - 1]}} \quad (13)$$

For  $T_e/T_n = 2$ , Eq. (13) reduces to

$$\frac{j}{\sigma_p} = 4.06 \times 10^{16} P_n \left( \frac{\delta T_e}{M_n T_n} \right)^{1/2} \sum_i X_i Q_{ei} \frac{\text{v}}{\text{cm}} \quad (14)$$

where  $P_n$  is in atmospheres,  $\delta$  is dimensionless,  $T_e$  and  $T_n$  is in degrees Kelvin,  $X_i$  is dimensionless, and  $Q_{ei}$  is in square centimeters.

#### References

- <sup>1</sup> Hurwitz, H., Jr., Sutton, G. W., and Tamor, S., "Electron heating in magnetohydrodynamic power generators," *ARS J.* **32**, 1237 (1962).
- <sup>2</sup> Massey, J. and Burhop, E., *Electronic and Ionic Impact Phenomena* (Oxford University Press, London, 1952).